

KgpKubs 2018 Team Description Paper

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Abstract. This paper describes the mechanical, electronic and software designs developed by Kharagpur RoboSoccer Students' Group (KRSSG) team to compete in RoboCup 2018. All designs are in agreement with the rules and regulations of Small Size League 2018. Software Architecture implemented over Robot Operating System(ROS), trajectory planning and velocity profiling, dribbler/kicker design and embedded circuits over the last year have been listed.

1 Introduction

KgpKubs is a RoboSoccer team from IIT Kharagpur, India. The research group aims to make autonomous soccer playing robots and participate and conduct various related events. Undergraduate students from varied departments and years are a part of this group. We have previously participated in FIRA RoboWorld Cup in the years 2013-2015 in the Mirosot League and secured Bronze Medal in the same in 2015. We have also participated in RoboCup SSL & 3D-Simulation League in Nagoya, Japan 2017. In December 2017 we participated in RoboCup Asia-Pacific in Thailand in the 3D-Simulation League.

This paper is a continuation of last year's Team Description paper and describes the developments made after last year's participation. Mechanical design of the robots is presented in section 2. The firmware and embedded circuits are described in section 3, followed by the software system in section 4. Finally, the discussion and future work are described in section 5.

2 Mechanical Design

The robots are designed in Solidworks. Extensive simulation and testing were done using Ansys (Workbench) and Adams to validate the results.

The robot chassis is manufactured using Aluminium 6061 to ensure the strength of the robot and keep it low weight. All the electrical components

are organized in a housing compartment which ensures safety and accessibility inside the robot. Table 1 summarizes hardware configuration of the bot.

Table 1: Robot Hardware

Dimensions	Dia: 179mm , Height: 149mm
Driving motors	Maxon EC-45 Flat (50W)
Gear Type	Internal Spur
Gear Ratio	1:3.3
Wheel diameter	50mm
Dribbling motor	Maxon EC-16 (30W)
Dribbling gear Ratio	2:1
Dribbling bar diameter	Dia: 14mm
Max. ball coverage	19%
Sub-wheel Diameter	10mm

2.1 Locomotion System

The drive system is a four-wheel omni-drive with the rear wheels inclined at 90 degrees and the front wheels inclined at 120 degrees to provide space for the dribbler and kicker mechanism. The motor used for driving is Maxon EC45 (50W). Spur gears are used between wheels and motors with a gear ratio of 1 : 3.3. A significant drawback in last year's robot was the loosening of screws joining the wheel and the shaft after a few minutes of continuous motion. So we redesigned the washer and implemented a new square locker mechanism to correct this problem.

2.2 Dribbling Mechanism

In the previous design, the major problem was that of the ball getting under the dribbler which induced a tendency of backward toppling in the robots. It was fundamentally because of the following two reasons that there occurred incorrect torques and impulsive reaction forces,

1. The dribbler rod was not at the correct height from the ground.
2. The dribbler had an angular suspension, as a result when it damped the incoming ball, the angle of contact between the ball and the dribbler changed.

The dribbler would lose contact with the ball due to vibrations and insufficient damping. Hence, we completely remodelled our dribbler.

The new model shown in Fig.1, has been engineered to have a linear damping mechanism. It damps by moving horizontally backwards while receiving the ball. In this mechanism, the angle of contact remains constant. In addition to it, an angular mechanism has been implemented so that the height of the dribbler rod

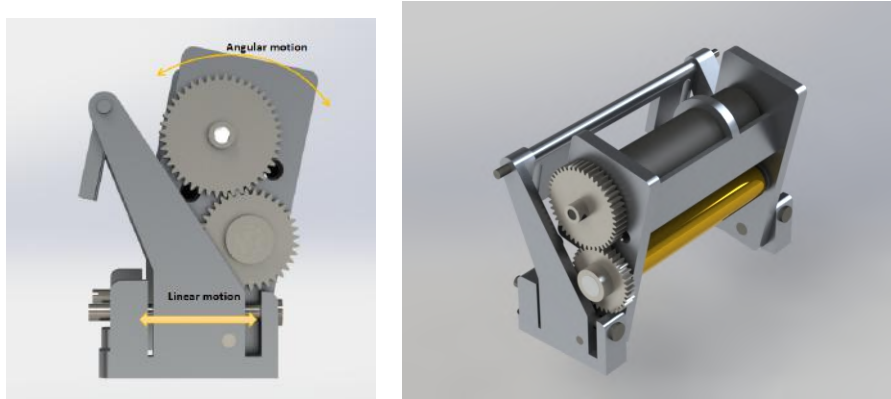


Fig. 1: CAD Model of the new Dribbler

can be changed. This helps in setting the best height for the dribbler rod as the environment changes so that it can dribble the ball efficiently. This further gives a decent range of backward and forward acceleration of the robot and hence it does not topple.

The dynamical equations were formulated for the active handling of the ball and hence, the best range of accelerations were attained from $-3m/s^2$ to $+3m/s^2$. Considering this range and including other factors like coefficient of friction between ball and ground and normal reaction between the ball and the dribbler rod, the best range of angle of contact was calculated and hence the best range for dribbler height. The best range of height for the dribbler rod from the ground is between $27.3mm$ to $29.3mm$. Additionally, The best range of angles is from 0° to 20° . All the results were attained by carrying out analysis in MATLAB.

Further calculations established that the best gear ratio with the motor Maxon EC16 30W and gear-box is $4.4 : 1$ which is $9 : 11$. For the dribbler material, silicon rubber has been used. Currently, our team is using the previous design in our robots, but the new design will be implemented before RoboCup 2018.

2.3 Kicking Mechanism

Straight Kicker

The straight kicker is powered by two 250V 2200uF capacitors, which can be charged by a step-up converter to 200V each. In the earlier design, we had cylindrical solenoids made of 6061-Aluminium alloy. It had windings of 23AWG copper wire and 680 turns. The design was good and sufficiently robust for kicking the ball up to 8 m/s, but had two major drawbacks:

1. Solenoid's frame was made of metal, which resulted in short-circuiting problems.
2. Cylindrical solenoids consume a lot of space, so implementing the same dimension of solenoids for both straight and chip kicker becomes difficult.

So, to tackle the problems mentioned above and keeping in mind the performance of the solenoid, optimization analysis was carried out using MATLAB. Also, the solenoid's frame would be made out of Polyoxymethylene (POM), which has high structural strength, high stiffness and low coefficient of friction, hence making it ideal for this purpose.

Solenoid Optimization

The goal was to achieve maximum energy generation by the solenoid while keeping the dimensions as a constraint. In order to efficiently use the space available, a rectangular cross-section has been used for the solenoid. The outer dimensions were decided by maximising the volume of solenoids within the available space. Optimization of the inner dimensions was carried out by implementing Finite Element Analysis using MATLAB. The magnetic field was calculated for each elemental volume inside the solenoid and integrated over the volume of the solenoid to get the total flux through the solenoid. By varying the dimensional parameters and taking 23 AWG wire for the winding, due to its superior performance as mentioned in KPGKubs TDP 2017 [13], the graph of Magnetic flux vs breadth vs width of the solenoid was plotted. From the graph, we found that the flux is maximum for $l \times b \times h = 56mm \times 40mm \times 18mm$. Further, the thickness of the winding layers is $3.4mm$ which sets the inner dimensions of the solenoid.

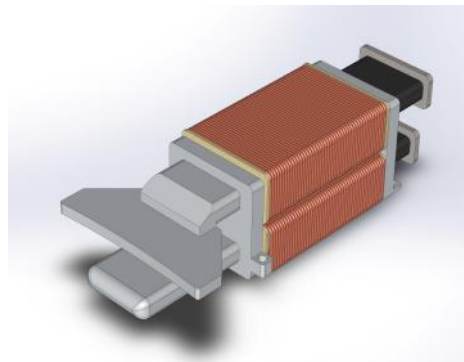


Fig. 2: CAD Model of the new Kicker Module

3 Embedded System

3.1 Main controller board

STM32F407VG is used as the processing unit which controls four base motors, dribbler and other peripherals. The communication between the main board and computer is established using Nordic nRF24L01+ radio modules. For accurate kicking, TSOP IR obstacle sensor module has been used to sense the appropriate location of the ball before kicking.

In our previous participation a few problems were recognized like wheel slipping, LiPo overdischarge, and difficulties in programming STM using STLink connectors. To tackle wheel slipping an onboard SD Card have been installed for real-time data logging of the encoder data. Lithium Polymer (LiPo) overdischarge protection circuit is incorporated in the main circuit. The onboard programming circuit is in the prototyping phase so that our main board can be directly programmed using the USB cable.

3.2 Power Circuit

A 5-cell 2200mAh LiPo battery is used to power the main controller and the kicker board. In the previous circuit, a comparatively bigger switch was used to turn ON/OFF the power supply. The switch was not robust, resulted in spark and would get damaged on a regular basis. In the present circuit, a relay based switch is integrated because of its low cost, low maintenance and sturdiness.

3.3 Motor Controllers

Currently, ESCON 24/2 motor controller module is used to control the four 50W and one 30W BLDC motors used in our robots. These controllers come with a dedicated microcontroller to drive the motor along with great error detection capabilities. The controller throws a lot of error and is not much reliable for the dynamic gameplay involved in SSL. The drivers needs to be replaced, the four mentioned motors drivers have been tested successfully.

1. The UC2950 is a Texas Instrument (TI) based IC provides high-current switching with low saturation voltages when activated by low-level logic signals. This driver has the high current capability to drive large capacitive loads with fast rise and fall times; but with high-speed internal flyback diodes, it is also ideal for inductive loads.
2. The IR4427 is a low voltage, high-speed power MOSFET and IGBT driver. The output drivers feature a high pulse current buffer stage designed for minimum driver cross-conduction. Propagation delays between two channels are matched. IR4427 was initially tested with N-MOS IRF540N and P-MOS IRF940N. Optimal results were observed. Then the testing with IRF7389 was initiated but the results were not acceptable.

3. The MC33035 is a high-performance second generation monolithic brushless DC motor controller containing all of the active functions required to implement a full-featured open loop, three or four phase motor control system (closed loop can be implemented using a companion IC MC33039). This device consists of a rotor position decoder for proper commutation sequencing; temperature compensated reference capable of supplying sensor power, frequency programmable sawtooth oscillator, three open collector top drivers, and three high current totem pole bottom drivers ideally suited for driving power MOSFETs. MC33035 was initially tested with N-MOS IRF540N. Optimal results were observed.
4. The A3930 is a three-phase brushless DC (BLDC) motor controllers which can be used with N-channel external power MOSFETs. They incorporate much of the circuitry required to design a cost-effective three-phase motor drive system and have been specifically designed for automotive applications. It was initially tested with N-MOS IRF540N. Optimal results were observed.

Further testing is being done on above-mentioned circuits. The best circuit will be incorporated into the main circuit.

3.4 Communication Module

Bi-directional communication have been established between the base station and the robots. Each robot has three nRF24L01+ chips connected on board. Out of three, two are used for receiving data, as opposed to only a single nRF24L01+ chip, and this minimizes data loss. The third nRF24L01+ chip is used to send data back to the base station from each of the robots. The base station too has two nRF24L01+ chips to receive data from the robots. The multiple data-pipes is being used in the nRF24L01+ to receive data from all the robots at the same time. So, this year, the nRF24L01+ chips have been soldered directly on the main circuit, as opposed to using female berg strips, and this prevents it from getting loose when subjected to collisions and vibrations, which was one of the major issues of the previous generation robots.

3.5 Kicker Board

The kicker board constitutes of charging and discharging circuit. The circuit has a dedicated ATmega328 microcontroller. The board receives external interrupt trigger and kicking level from the main circuit. The Kicker board charges two 2200uF capacitors using flyback topology up to 200V each. This year the design of circuit has been changed completely. The previous circuit occupied a lot of space, produced electric sparks and required excessive maintenance. Also the charging time of the capacitor was more as compared to the new circuit.

Charging Circuit

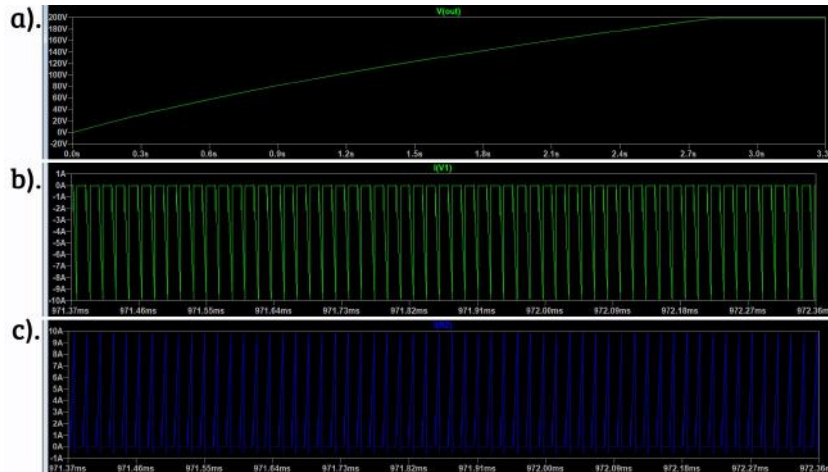


Fig. 3: a) Capacitor Voltage vs Time
 b) Supply Current vs Time
 c) Charging Current vs Time

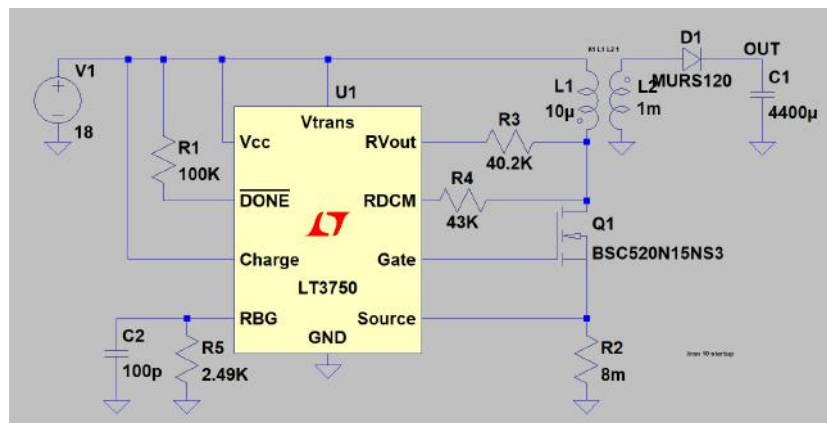


Fig. 4: Flyback converter circuit using LT3750

The earlier charging circuit was based on Switch Mode Power Supply (SMPS) and used flyback converter to charge two 2200uF capacitors to 150 volts in six-seven seconds. For switching, Power MOSFETs were used which were controlled by a PWM signal from Atmega with a frequency of 100 kHz. But the circuits were not robust, MOSFETs were damaged frequently and charging time was high which prevented us from kicking frequently. So to improve our circuit and rectify all the problems we switched to LT3750, a capacitor charge controller from linear technology. The LT3750 is a flyback converter designed to rapidly charge large capacitors to a user-adjustable target voltage. It consists of a different

resistor which can be used to change various output parameters like charging current. The CHARGE pin on the IC gives full control of the LT3750 to the user and the DONE pin indicates when the capacitor has reached its programmed value, and the part has stopped charging. It also has features like under voltage lockdown and overvoltage protection. Simulations on LTSpice shown in Fig.3 showed improved efficiency and reduced charging time. The new charging circuit is significantly small in size and much more robust and faster than the previous circuit.

Discharging Circuit

In the current circuit, capacitors were discharged using relays through a solenoid because of which capacitors can only be discharged at three different levels, and switching losses were high. Relays used to burn due to a high discharging current flowing through them. To overcome these problems two different circuits were tested for discharging capacitors. In the first circuit, capacitors are discharged using IGBT IGB50N60T which is driven using an optocoupler HCPL-3120. In the second circuit, capacitors are discharged through a power MOSFET IRFS4127 which is operated using gate driver TC4426 which is, in turn, connect to Atmega through an optocoupler HCPL-817. Both the circuits are tested for variable discharging capacitors, and both are working fine. The switching and transient losses of both the circuits will be compared and the best one will be incorporated in final discharging circuit.

Communication with Main Circuit

Earlier kicker circuit was controlled by interrupts from the main circuit. There was a problem of false interrupts which results in unnecessary kicking. So in this version, UART is used as the mode of communication between main board and kicker. On top of that one more verification mechanism is implemented to eliminate the possibility of unnecessary kicking.

4 Software

The following section has the description of the developments and changes made on the software side, since our last participation in SSL. An overview of Finite State Machine (FSM) architecture developed on Robot Operating System (ROS) is presented in subsection 1. Subsection 2 discusses the improvements in vision data processing for updating the world state model. Subsection 3 analyses the controls and the various methods applied for PID tuning. Subsection 4 discusses our GUI development for testing and tuning robots. Subsection 5 is about path planning, mainly the RRT and its variants. Subsection 6 highlights our work on velocity profiling.

4.1 Code Base

This paper proposes Finite State Machine (FSM)[16] developed on ROS for implementing adaptive robot behaviours. Our software relies on deterministic finite automaton implemented through FSM. This is a generic hierarchical state machine class in which a state comprises of sub-states. Each state is implicitly in its parent state, thus sufficing the polymorphism of state machines.

There are three methods corresponding to each STATE:

- **on_enter_STATE**
- **execute_STATE**
- **on_exit_STATE**

Each transition edge calls on_exit function on parent's state followed by on_enter and execute function on its unique child's state. Recursive transitions between states continue until an action has met its target state or termination. Failure of any transition leads to termination.

Issues:

Our previous RoboSoccer software based on naive Skill Tactic Play (STP) architecture had several issues :

1. Intercommunication between various skills, tactics and plays was limited, resulting in inefficient coordination between agents.
2. For testing a single part of the code, the whole project had to be re-compiled and executed, thus limiting the scope of unit testing.
3. All the computations were made on each video frame due to an inefficient structure of the code, making it slow.

Developments:

Software developed on Finite State Machine has the following improvements:

1. Independent testing for each Role, Action and Play.
2. Computations are currently performed only during the strategic transition of every state.
3. The execution of complex strategies has been simplified into a composed form of low-level actions.

Modules:

- **state_machine** comprises the architecture of finite state machine
- **roles** comprises definitions of simple motions.
- **actions** consists of definitions of collection of roles.
- **plays** comprises definitions of plays.
- **planners** contains definitions of path planners and controllers used by roles.

- **belief_state** subscribes to SSL-Vision and publishes Belief State information on belief_state topic. It includes state of robots and ball along with field parameters and predicates. The state comprises the position and velocity vectors.

- **ssl_common** contains miscellaneous libraries that are required by several modules such as configuration files, network libraries, serializerdeserializer etc.

- **ssl_msgs** contains all ROS message definitions required by other modules. Communication on all topics must be through one of these message types.

- **vision_comm** describes node that publishes vision information to the topic vision and connects to either SSL Vision instance (real robots) or grSim instance(simulator) depending on execution parameters.

- **kgpkubs_launch** contains launch files and other scripts for launching all nodes on a machine.

- **navigation** contains executables for path planners and PID which are used for locomotion.

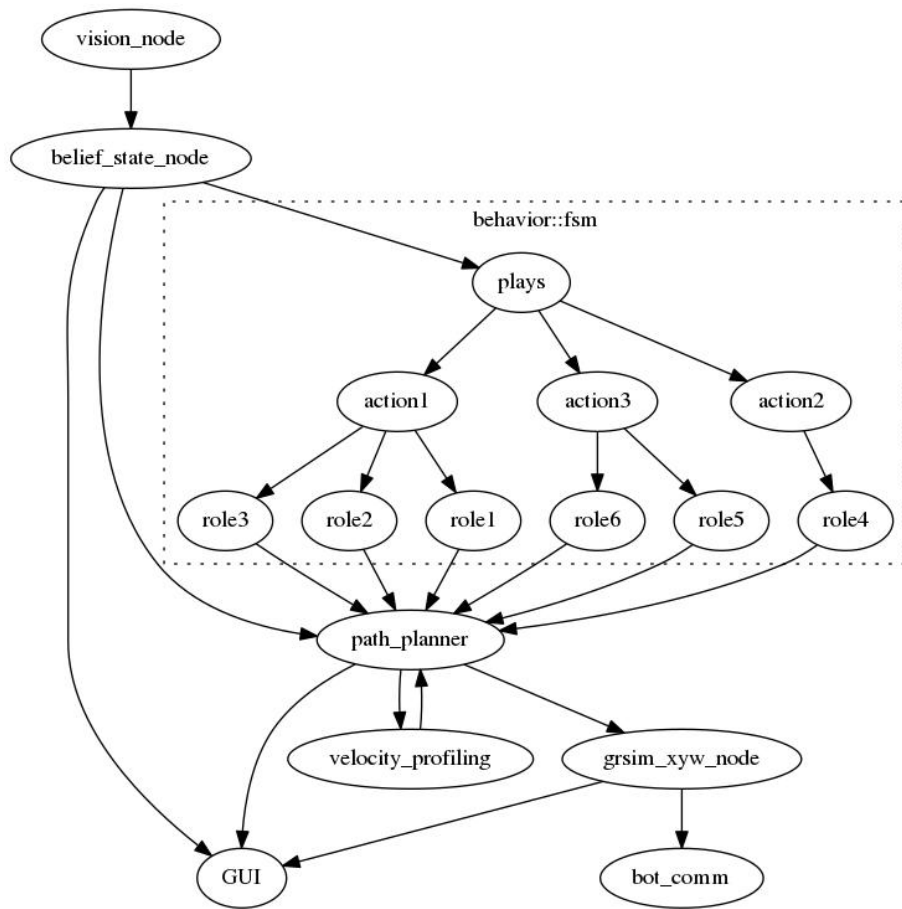


Fig. 5: RoboSoccer software architecture

4.2 Vision

The data captured by the camera is not reliable as it is noisy. This hinders the prediction of robots' positions and velocities accurately. To overcome this problem we tested two filters - the Savitzky-Golay filter and Kalman filter. Though the results obtained from both the filters were almost the same, the Kalman filter was a tad slower and resource heavy as compared to the Savitzky-Golay filter. So, we used Savitzky-Golay filter to keep up with the frame rate.

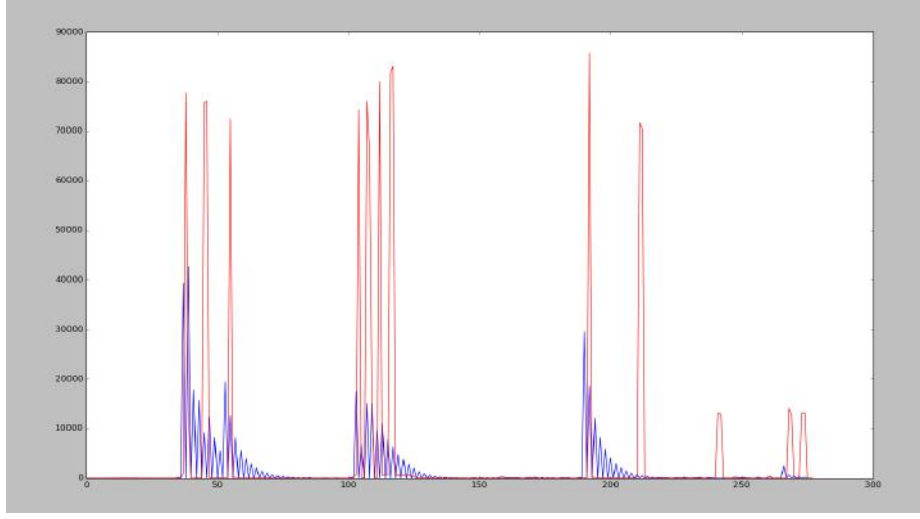


Fig. 6: Red Line - Unfiltered absolute velocity data, Blue Line - Filtered absolute velocity data

4.3 PID Control

PID controller [14] calculates and rectifies error in position of robots and applies a correction using proportional, integral and derivative parameter. We have applied this controller to position error of robots independently in the x and y coordinates.

$$\vec{e} = \overline{SP} - \overline{CP} \quad (1)$$

\mathbf{e} is the error in position vector, \overline{SP} is the set point, \overline{CP} is the current point

Parameters of PID controller were tuned to minimize rise time, overshoot and remove steady-state error in the position of a robot.

For optimizing parameters, Trial & Error and Particle Swarm Optimization (PSO) [15] were tried. In PSO, a swarm of particles is created whose position is initialised randomly in the environment representing constants of PID Controller. Each particle moves based on the best global position of swarm and best local position of particle.

$$v_i(t+1) = wv_i(t) + c_1r_1[\hat{x}_i(t) - x_i(t)] + c_2r_2[g(t) - x_i(t)] \quad (2)$$

\mathbf{i} is the particle index, \mathbf{w} is inertial coefficient, c_1, c_2 are acceleration coefficients, r_1, r_2 are random values.

For Trial & Error optimization, initially, PID parameters are set to zero. The proportional parameter of PID is increased till steady oscillations are achieved. Consequently, the derivative setting is increased to minimize oscillations in error. The integral parameter of PID is then used to minimize steady state error if any.

$$u(t) = k_p e(t) + k_i \int_0^t e(t') dt' + k_d \frac{d(e)}{dt} \quad (3)$$

4.4 GUI Development

We developed a PyQt based GUI for testing and analysing the performance of variants of the Rapidly Exploring Random Tree (RRT) algorithm. This GUI makes it simple and time efficient to monitor the errors.

Features:

- To test Basic Skills
- Real time analysis of growing tree for various RRT algorithms



4.5 Path Planning

A few path planners were implemented which suited our purposes, including variants of RRT and Kinodynamic planners. Kinetics and dynamics of the robot were difficult to capture in kino-dynamic planners. Hence, we focused on variants of RRT, specifically RRT Connect, Real-Time RRT Star (RT-RRT* with edge re-wiring [17]) and RRT Star (RRT*). The efficiency of these planners over the other variants was determined using some preliminary tests. They were developed and

integrated with ROS and our GUI. Exhaustive testing on grSim and the robots were done. After generation of a path, it is processed using multiple steps of simplifications and smoothing. In Table 2 we present a set of planners and the time required for path generation and simplification. Figure 7 shows the tree growth and paths formed by the RRT algorithms.

Table 2: Path planners

Planner	Solution time (in s)	Simplification time (in s)
RRT	0.001284	0.002113
RRT Connect	0.000677	0.001080
RT-RRT Star	0.000732	0.000963
RRT Star	5.004750	0.000203
LBT RRT	5.000386	0.000319
Lazy RRT	0.047412	0.000328
TRRT	0.014794	0.001864
pRRT	0.001266	0.000875
Informed RRT Star	5.000174	0.000252

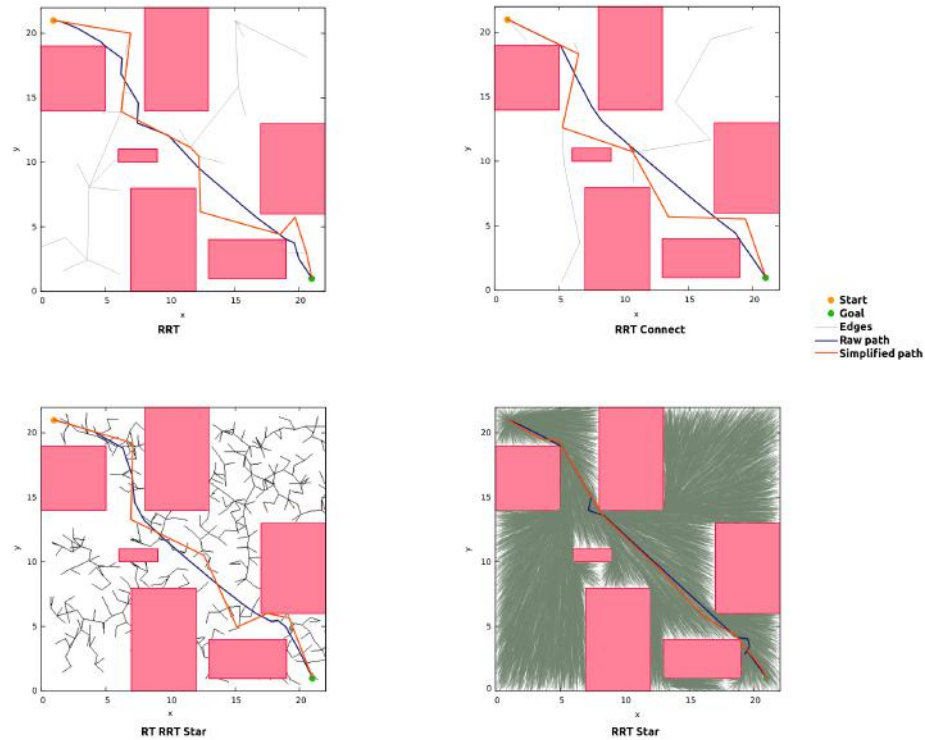


Fig. 7: Various path planners implemented under similar environmental states

4.6 Velocity Profiling

After a detailed analysis of the speed, the performance of S-curve and Trapezoidal Velocity Profile we have implemented the latter one. With adaptive restrictions on Max Velocity and acceleration, it creates a velocity-time mapping for given path, which is used to predict velocity at any instant, meant to be modified by PID after taking in considerations the error in current and expected positions. (Refer Section 4.3).

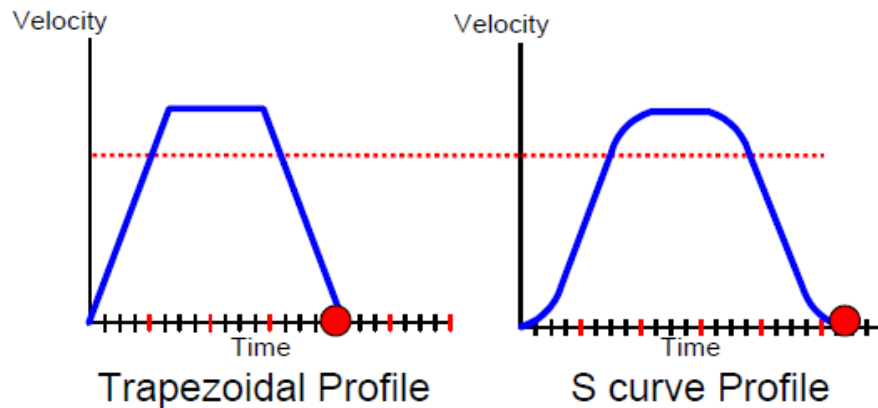


Fig. 8: Trapezoidal and S curve velocity profiling

5 Discussion and Future Works

As future work, it is imperative to explore more dynamics that affect the robot behaviour. On the embedded side, we aim to incorporate variable discharging for controlling the speed with which ball is hit; develop fuzzy-PID controller based on encoder readings; integrate IMU for better state estimation. On the software side, we would improve upon the tracking algorithm and upgrade inter-tactic strategies such as pass-receive.

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